

D01- GENERAL

D01-1 GENERAL INFORMATION

1. THE INFORMATION PRESENTED ON THESE DRAWINGS HAS BEEN DESIGNED AND ANALYZED IN ACCORDANCE WITH THE 2012 (R22) ONTARIO BUILDING CODE & 2015 NATIONAL BUILDING CODE OF CANADA. CONSTRUCTION IS TO BE PERFORMED IN ACCORDANCE WITH THIS AND ALL OTHER APPLICABLE CODES.
- 1.1 CONCRETE STRUCTURE DESIGNED IN ACCORDANCE WITH CSA A23.3-14
 - 1.2 STEEL STRUCTURE DESIGNED IN ACCORDANCE WITH CAN/CSA-S16-14
 - 1.3 WOOD STRUCTURE DESIGNED IN ACCORDANCE WITH CAN/CSA-086-14
 - 1.4 MASONRY STRUCTURE DESIGNED IN ACCORDANCE WITH CAN/CSA S304-14
2. ALL WORK MUST COMPLY WITH THE PROVISIONS OF THE 2012 (R22) ONTARIO BUILDING CODE, OCCUPATIONAL HEALTH & SAFETY ACT, MUNICIPAL BYLAWS AND BEST CODE PRACTICES. THE CONTRACTOR MUST CONSIDER THAT CONSTRUCTION WORK IS DEPENDENT ON SITE CONDITIONS.
3. ALL DIMENSIONS ARE IN MILLIMETRES AND ELEVATIONS IN METRES UNLESS INDICATED OTHERWISE.
4. GUARDRAILS / HANDRAILS SHALL BE DESIGNED AND CERTIFIED BY THE FABRICATOR'S PROFESSIONAL ENGINEER LICENSED IN ONTARIO IN ACCORDANCE WITH LOADS PROVIDED IN THE 2012 (R22) ONTARIO BUILDING CODE / 2015 NATIONAL BUILDING CODE. STAMPED SHOP DRAWINGS TO BE SUBMITTED.
5. THE ROOF HAS BEEN DESIGNED FOR THE REQUIRED STORM WATER FLOW RESTRICTION IN ACCORDANCE WITH 2012 (R22) ONTARIO BUILDING CODE REQUIREMENTS.
6. CONTRACTOR IS TO VERIFY / COORDINATE ALL DIMENSIONS / PENETRATIONS WITH ARCHITECTURAL / MECHANICAL / ELECTRICAL DRAWINGS PRIOR TO CONSTRUCTION. REPORT INCONSISTENCIES BEFORE PROCEEDING WITH WORK. ANY OPENINGS NOT INDICATED ON STRUCTURAL DRAWINGS ARE TO BE APPROVED BY STRUCTURAL ENGINEER IN WRITING PRIOR TO CONSTRUCTION.
7. CAD / REVIT VERSIONS OF THE STRUCTURAL DRAWINGS SHALL BE MADE AVAILABLE TO THE CONTRACTOR UPON THE COMPLETION OF A RELEASE FORM INDEMNIFYING THE CONSULTANT FROM ANY ERRORS OR OMISSIONS ASSOCIATED WITH THE CAD / REVIT FILES.
8. LADDERS SHALL BE DESIGNED AND CERTIFIED BY THE FABRICATOR'S PROFESSIONAL ENGINEER LICENSED IN ONTARIO IN ACCORDANCE WITH LOADS PROVIDED IN PART 4 AND PART 3 OF THE 2012 (R22) ONTARIO BUILDING CODE / 2015 NATIONAL BUILDING CODE. STAMPED SHOP DRAWINGS TO BE SUBMITTED.
9. STEEL STAIRS SHALL BE DESIGNED AND CERTIFIED BY THE FABRICATOR'S PROFESSIONAL ENGINEER LICENSED IN ONTARIO IN ACCORDANCE WITH LOADS PROVIDED IN PART 4 AND PART 3 OF THE 2012 (R22) ONTARIO BUILDING CODE / 2015 NATIONAL BUILDING CODE. STAMPED SHOP DRAWINGS TO BE SUBMITTED.
10. DEMOLITION DETAILS THAT AFFECT THE STRUCTURAL ELEMENTS HAVE BEEN REVIEWED IN ACCORDANCE WITH THE 2012 (R22) ONTARIO BUILDING CODE. WHERE REQUIRED, SUPPLEMENTARY / TEMPORARY / REMEDIAL FRAMING HAS BEEN PROVIDED.
11. SEISMIC RESTRAINT OF ARCH / MECH / ELECT ELEMENTS NOT NOTED ON THE DRAWINGS ARE THE RESPONSIBILITY OF THE CONTRACTOR'S ENGINEER. RESTRAINT DETAILS ARE TO BE DEVELOPED IN ACCORDANCE WITH THE 2012 (R22) ONTARIO BUILDING CODE. CONTRACTOR'S ENGINEER IS RESPONSIBLE FOR THE DESIGN AND DETAILING OF SEISMIC RESTRAINTS AND ISOLATIONS AS REQUIRED BY SPECIFICATIONS INCLUDING THE VERIFICATION THAT THE EXISTING / NEW STRUCTURE IS CAPABLE OF SAFELY SUPPORTING THE IMPOSED LOADS IN ACCORDANCE WITH THE 2012 (R22) ONTARIO BUILDING CODE. NO ELEMENTS MAY BE CONSTRUCTED WITHOUT WRITTEN CONFIRMATION OF THESE CONDITIONS BY CONTRACTOR'S ENGINEER.
12. NO FOUNDATION ELEMENTS ARE TO BE CONSTRUCTED UNTIL WRITTEN APPROVAL OF THE BEARING SURFACES AND PRESSURES IS PROVIDED BY A GEOTECHNICAL ENGINEER THROUGH ON-SITE INVESTIGATION. FAILURE TO COMPLETE THIS WORK COULD RESULT IN THE REMOVAL / REINSTATEMENT OF ANY / ALL FOUNDATION ELEMENTS AT CONTRACTOR'S OWN COST.
13. NEW OPENINGS IN EXISTING / ERECTED CONCRETE / MASONRY ELEMENTS:
- REFER TO MECH / ARCH / ELECT DRAWINGS FOR LAYOUTS.
 - SCAN T&B / E.S. OF SLAB/WALL PRIOR TO REMOVALS. MARK OUT OPENING POSITION/ALL REBAR/CONDUIT ON T&B OF SLAB / E.S. OF WALL MIN. OF 4 WEEKS PRIOR TO REINFORCING SHOP DRAWING SUBMISSION / CUTTING / CORING.
 - CONTACT ENGINEER FOR REVIEW OF SCANS/MARKS PRIOR TO COMMENCEMENT OF ANY DEMOLITION.
 - NO WORK TO COMMENCE UNTIL RECEIVING WRITTEN APPROVAL FROM ENGINEER.
 - SAWCUT/CORE OUT OPENINGS AS REQUIRED.
 - DO NOT OVERCUT.
 - ANY REQUIRED SUPPLEMENTAL STRENGTHENING/REINFORCING IS TO BE ERECTED PRIOR TO REMOVALS.
14. CONTRACTOR TO PROVIDE PRE-ENGINEERED SHORING AS REQUIRED TO ACCOMMODATE THE CONTRACTOR'S CONSTRUCTION ACTIVITIES AND TO PREVENT DAMAGE TO ANY ADJACENT PROPERTY. ALL CONSTRUCTION ACTIVITIES TO BE LIMITED TO THE LIMITS OF THE CONSTRUCTION SITE AND ALL DAMAGE TO EXISTING PROPERTIES MUST BE REINSTATED.
15. CONTRACTOR IS REQUIRED TO SUBMIT CONDUIT AND SLEEVING SHOP DRAWINGS FOR ALL FLOORS / ROOFS / WALLS / COLUMNS PRIOR TO THE ERECTION / CONSTRUCTION / FABRICATION OF ANY OF THESE ELEMENTS. THE DRAWINGS ARE TO LOCATE / DIMENSION THE CLEAR SIZES OF OPENINGS / SLEEVES / CONDUITS IN PLAN (FLOORS / ROOFS / COLUMNS) AND ELEVATION (WALLS / BEAMS). THE COORDINATION OF THE VARIOUS DISCIPLINES / SUBTRADES TO ENSURE ALL ITEMS ARE CLEARLY INDICATED IS THE SOLE RESPONSIBILITY OF THE CONTRACTOR. DRAWINGS ARE TO BE SUBMITTED A MINIMUM OF 4 WEEKS PRIOR TO THE CONSTRUCTION OF THE AFFECTED ELEMENT.
16. DO NOT SCALE DIMENSIONS DIRECTLY FROM THESE DRAWINGS OR ELECTRONIC FILES.
17. SPECIFIC NOTES AND DETAILS FOUND ON THESE DRAWINGS SHALL TAKE PRECEDENCE OVER GENERAL NOTES AND TYPICAL DETAILS.
18. DO NOT LOAD HEAVY MATERIALS SUCH AS MASONRY, FILL, GRAVEL, DRYWALL, ETC. ON FLOORS, TERRACES OR ROOFS WITHOUT ADEQUATE ADDITIONAL SUPPORTS. SUBMIT DETAILS TO ENGINEER FOR REVIEW.

D01-2 DESIGN LOADS:

IMPORTANCE FACTORS:

SNOW: I_s ULS= 1.0 SLS= 0.9
WIND: I_w ULS= 1.0 SLS= 0.75
SEISMIC: I_s ULS= 1.0

SNOW LOAD FACTORS:

$S = I_s [Sw(Cb^2 Cw^2 Cs^2 Ca) + Sr]$
 $S_b = 2.4 \text{ kPa}$
 $S_r = 0.4 \text{ kPa}$
 $C_b = 0.8$
 $C_w = 1.0$
 $C_s = 1.0$

D01-3 SEISMIC SYSTEM/LOADING DATA

SEISMIC FORCE RESISTING SYSTEM (SFRS)

SFRS: SYSTEM & CONNECTIONS: (OBC 2012 (R22) CLAUSE 4.1.8.9/4.1.8.10)
LATERAL LOAD RESISTING SYSTEM: CONCRETE SHEAR WALLS, CONVENTIONAL CONSTRUCTION
 $R_d = 1.5$
 $R_o = 1.3$
CSA STANDARD: CAN/CSA A23.3-14
APPLICABLE CLAUSE(S): 21

SFRS: DIAPHRAGMS & CONNECTIONS: (OBC 2012 (R22) CLAUSE 4.1.8.15)
CSA STANDARD: CAN/CSA A23.3-14
APPLICABLE CLAUSE(S): 21

SFRS: SYSTEM FOUNDATIONS: (OBC 2012 (R22) CLAUSE 4.1.8.16)
CSA STANDARD: CAN/CSA
APPLICABLE CLAUSE(S): □ FOR ANCHORED FOOTINGS
■ FOR UNANCHORED FOOTINGS

CONFIRMATION: FOUNDATIONS HAVE BEEN DESIGNED TO RESIST THE LATERAL FORCES APPLIED TO THE SFRS IN ACCORDANCE WITH THE OBC 2012 (R22) INCLUDING ALL APPLICABLE AMPLIFICATION FACTORS.

SEISMIC IMPORTANCE FACTOR: (OBC 2012 (R22) CLAUSE 4.1.8.5)

$I_e = 1.0$

REFERENCE CITY: OTTAWA (M-C INTERNATIONAL AIRPORT)

SITE CLASS: THE NOTED SITE CLASSIFICATION FOR SEISMIC SITE RESPONSE AND SHEAR STRENGTH PARAMETERS INDICATED ARE AS REPORTED IN THE GEOTECHNICAL REPORT BY

□ A □ B □ C ■ D □ E □ F (SITE SPECIFIC SPECTRUM:)

PGA: 0.235 PGV: 0.199

PGA_{EFF}: (OBC 2012 (R22) CLAUSE 4.1.8.4(i))

$Sa(0.2) = 0.446$
 $PGA = 0.285$
 $= 1.56 < 2.0$

PGA_{IMP}: 0.285 PGA = 0.285

5% DAMPED SPECTRAL RESPONSE

ACCELERATION VALUES FOR REFERENCE CITY: (NATIONAL BUILDING CODE 2015 APPENDIX C)

$Sa(0.2) = 0.446$
 $Sa(0.5) = 0.240$
 $Sa(1.0) = 0.119$
 $Sa(2.0) = 0.056$
 $Sa(5.0) = 0.015$
 $Sa(10.0) = 0.0056$

DESIGN SPECTRAL RESPONSE ACCELERATION VALUES (DSRAV): (OBC 2012 (R22) CLAUSE 4.1.8.4)

$S(0.2) = 0.468$
 $S(0.5) = 0.302$
 $S(1.0) = 0.162$
 $S(2.0) = 0.0760$
 $S(5.0) = 0.0234$
 $S(10.0) = 0.00765$

SITE COEFFICIENTS: (OBC 2012 (R22) CLAUSE 4.1.8.4)

□ CLASS 'A': ($F_a = 0.69$ $F_v = 0.57$) □ CLASS 'B': ($F_a = 0.77$ $F_v = 0.63$) □ CLASS 'C': ($F_a = 1.0$ $F_v = 1.0$)

$F(0.2) = 0.69$
 $F(0.5) = 0.57$
 $F(1.0) = 0.57$
 $F(2.0) = 0.58$
 $F(5.0) = 0.61$
 $F(10.0) = 0.67$

$F(0.2) = 0.77$
 $F(0.5) = 0.65$
 $F(1.0) = 0.63$
 $F(2.0) = 0.63$
 $F(5.0) = 0.64$
 $F(10.0) = 0.69$

$F(0.2) = 1.0$
 $F(0.5) = 1.0$
 $F(1.0) = 1.0$
 $F(2.0) = 1.0$
 $F(5.0) = 1.0$
 $F(10.0) = 1.0$

CLASS 'D': ($F_a = 1.05$ $F_v = 1.36$)

$F(0.2) = 1.05$
 $F(0.5) = 1.26$
 $F(1.0) = 1.36$
 $F(2.0) = 1.41$
 $F(5.0) = 1.56$
 $F(10.0) = 1.39$

CLASS 'E': ($F_a = 1.16$ $F_v = 1.93$)

$F(0.2) = 1.16$
 $F(0.5) = 1.66$
 $F(1.0) = 1.93$
 $F(2.0) = 2.10$
 $F(5.0) = 2.29$
 $F(10.0) = 2.10$

SYSTEM RESTRICTION VALUE: $I_e Fa Sa(0.2) = 0.4688 \geq 0.35$ ■ YES □ NO

PERIOD DATA:

EMPIRICAL PERIOD: (OBC 2012 (R22) CLAUSE 4.1.8.11(3)) (a),(b) or (c)

$T_a(EMPIRICAL)_{NS} = 0.163 \text{ sec}$
 $T_a(EMPIRICAL)_{EW} = 0.163 \text{ sec}$

MODAL PERIOD: (OBC 2012 (R22) CLAUSE 4.1.8.11(3)(d) AND 4.1.8.3(8))

$T_a(MODAL)_{NS} = 0.325 \text{ sec}$
 $T_a(MODAL)_{EW} = 0.325 \text{ sec}$

DESIGN PERIODS/MODE & MOMENT FACTORS: (2012 (R22) OBC TABLE (4.1.8.11))

$S(0.2) = 21.6 \geq 8.0$ ■ YES □ NO

$T_a(DESIGN)_{NS} = 0.325 \text{ sec}$
 $T_a(DESIGN)_{EW} = 0.325 \text{ sec}$
 $M_v = 1.0$ $J = 1.0$
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DESIGN FUNDAMENTAL PERIOD BASED DSRAV: (OBC 2012 (R22) CLAUSE 4.1.8.11(2))

$S(T_a)_{NS} = 0.390$
 $S(T_a)_{EW} = 0.390$

IRREGULARITY REVIEW: (OBC 2012 (R22) TABLE 4.1.8.6)

1. VERTICAL STIFFNESS: □ YES ■ NO
2. WEIGHT: □ YES ■ NO
3. VERTICAL GEOMETRIC: □ YES ■ NO
4. IN PLANE DISCONTINUITY: □ YES ■ NO
5. OUT OF PLANE: □ YES ■ NO
6. WEAK STOREY: □ YES ■ NO
7. TORSIONAL: □ YES ■ NO
 $R_{tors} = 1.7$

NON-ORTHOGONAL: □ YES ■ NO

GRAVITY INDUCED LATERAL DEMAND IRREGULARITY □ YES ■ NO

CONCLUSION: BUILDING IS DYNAMIC ANALYSIS: DYNAMIC PROCEDURE METHOD: □ REGULAR □ IRREGULAR □ REQUIRED ■ NOT REQUIRED □ MODAL RESPONSE SPECTRUM □ NUMERICAL INTEGRATION TIME HISTORY □ N/A

TORSIONAL ECCENTRICITY: ■ ≥ 0.10 Dnx (4.1.8.11(10a)) $B \leq 1.7$ EQUIV. STATIC FORCE PROCEDURE) □ ≥ 0.10 Dnx (4.1.8.12(4a)) $B \geq 1.7$ ■ ≥ 0.05 Dnx (4.1.8.12(4b)) $B < 1.7$, 3-D DYNAMIC ANALYSIS(S)

STRUCTURAL SEPARATION: ■ THE ADJACENT STRUCTURES HAVE BEEN SEPARATED IN ACCORDANCE WITH 4.1.8.14(1) OF THE OBC 2012 (R22) □ N/A

BUILDING WEIGHT FOR SEISMIC DESIGN: $W = 1380 \text{ kN}$

BASE SHEAR/MOMENTS:

$V_{STATIC} = \frac{S(T_a)_{NS} \cdot I_e \cdot R_d \cdot W}{R_d \cdot R_o}$

STATIC MAXIMUM/MINIMUM VALUES:

NORTH-SOUTH: (↑↓)

$V_{MIN} = \frac{S(4.0) \cdot M_v \cdot I_e \cdot W}{R_d \cdot R_o} = W \cdot 0.0404 = 56 \text{ kN}$

$V_{MAX} = \left\{ \begin{array}{l} 0.66 \cdot \frac{S(0.2) \cdot I_e \cdot W}{R_d \cdot R_o} = W \cdot 0.16 = 220 \text{ kN} \\ 0.5 \cdot \frac{S(0.5) \cdot I_e \cdot W}{R_d \cdot R_o} = W \cdot 0.144 = 199 \text{ kN} \end{array} \right.$

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$V_{MAX} = \left\{ \begin{array}{l} 0.66 \cdot \frac{S(0.2) \cdot I_e \cdot W}{R_d \cdot R_o} = W \cdot 0.16 = 220 \text{ kN} \\ 0.5 \cdot \frac{S(0.5) \cdot I_e \cdot W}{R_d \cdot R_o} = W \cdot 0.144 = 199 \text{ kN} \end{array} \right.$

$V_{MAX} = \left\{ \begin{array}{l} 0.66 \cdot \frac{S(0.2) \cdot I_e \cdot W}{R_d \cdot R_o} = W \cdot 0.16 = 220 \text{ kN} \\ 0.5 \cdot \frac{S(0.5) \cdot I_e \cdot W}{R_d \cdot R_o} = W \cdot 0.144 = 199 \text{ kN} \end{array} \right.$

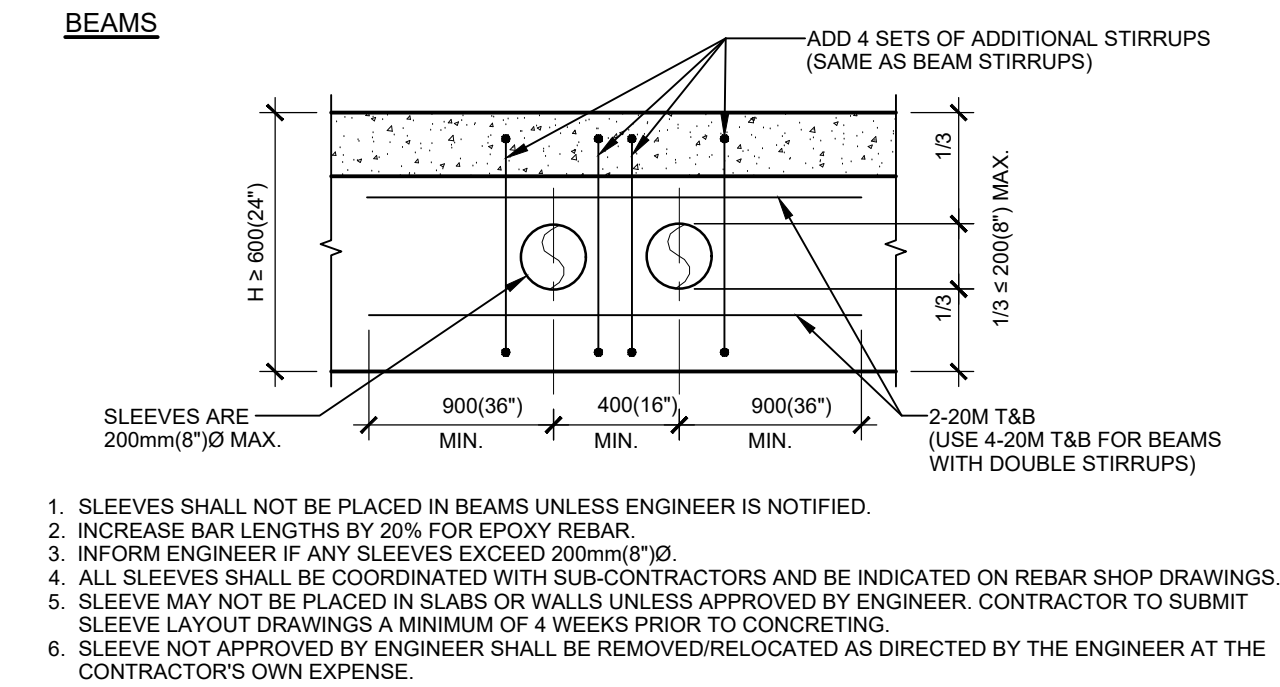
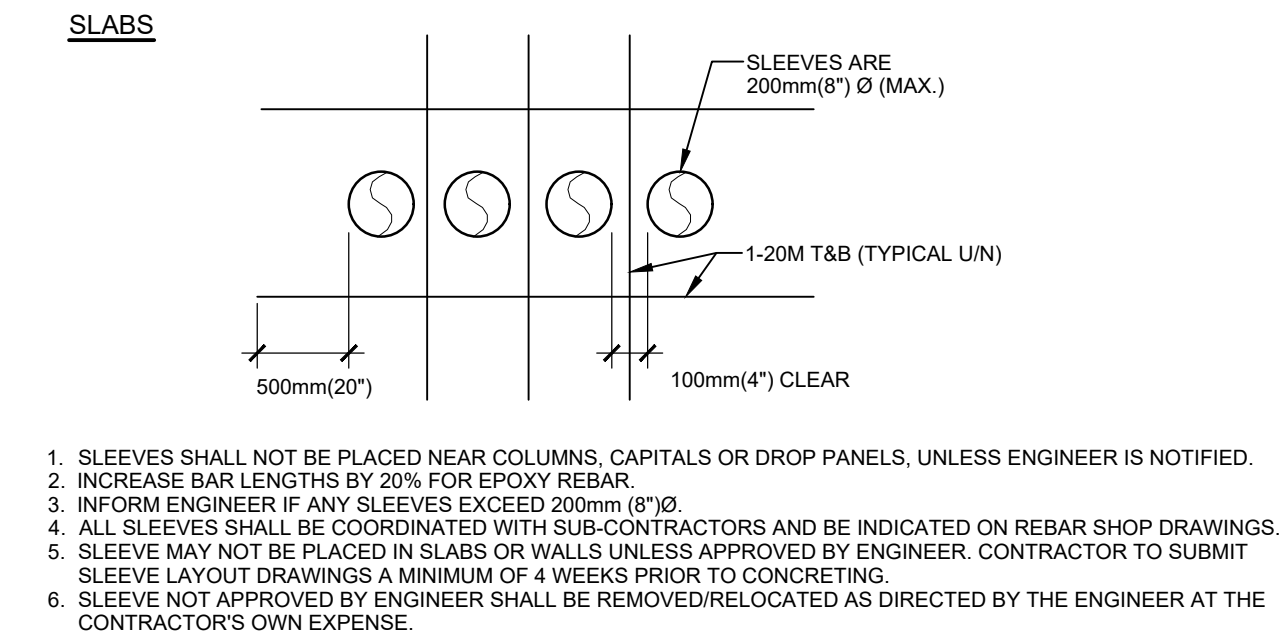
$V_{MAX} = \left\{ \begin{array}{l} 0.66 \cdot \frac{S(0.2) \cdot I_e \cdot W}{R_d \cdot R_o} = W \cdot 0.16 = 220 \text{ kN} \\ 0.5 \cdot \frac{S(0.5) \cdot I_e \cdot W}{R_d \cdot R_o} = W \cdot 0.144 = 199 \text{ kN} \end{array} \right.$

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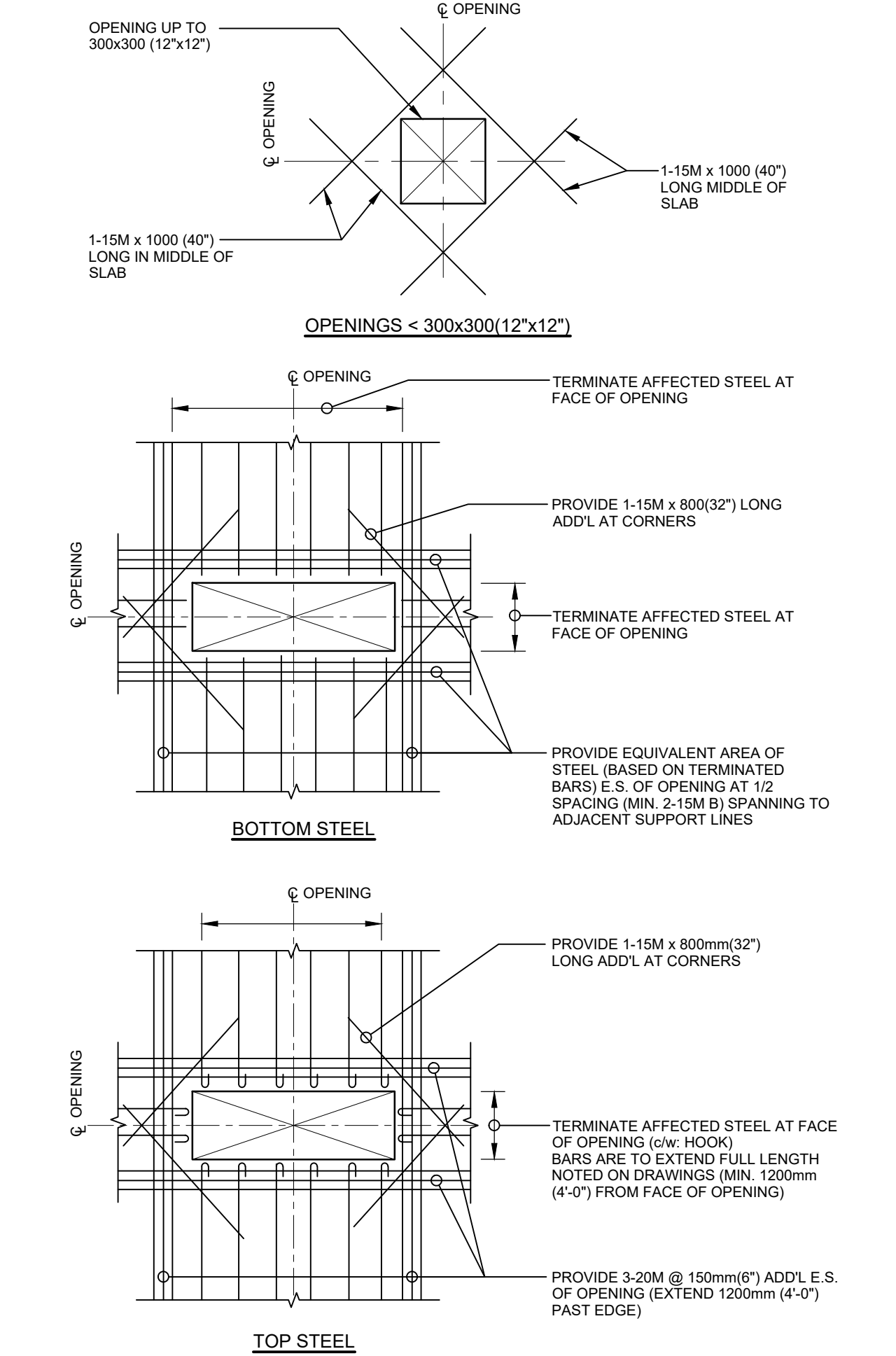
$V_{MAX} = \left\{ \begin{array}{l} 0.66 \cdot \frac{S(0.2) \cdot I_e \cdot W}{R_d \cdot R_o} = W \cdot 0.16 = 220 \text{ kN} \\ 0.5 \cdot \frac{S(0.5) \cdot I_e \cdot W}{R_d \cdot R_o} = W \cdot 0.144 = 199 \text{ kN} \end{array} \right.$

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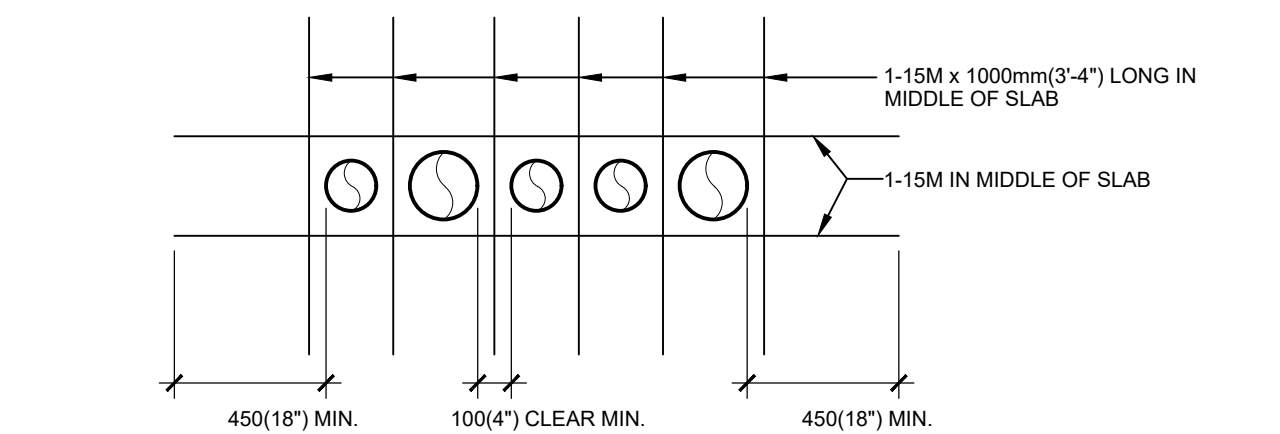
D03-23 SLEEVES THROUGH SLABS AND BEAMS



D03-24 TYPICAL TRIMMING DETAIL OF OPENING IN SLAB (U/N)



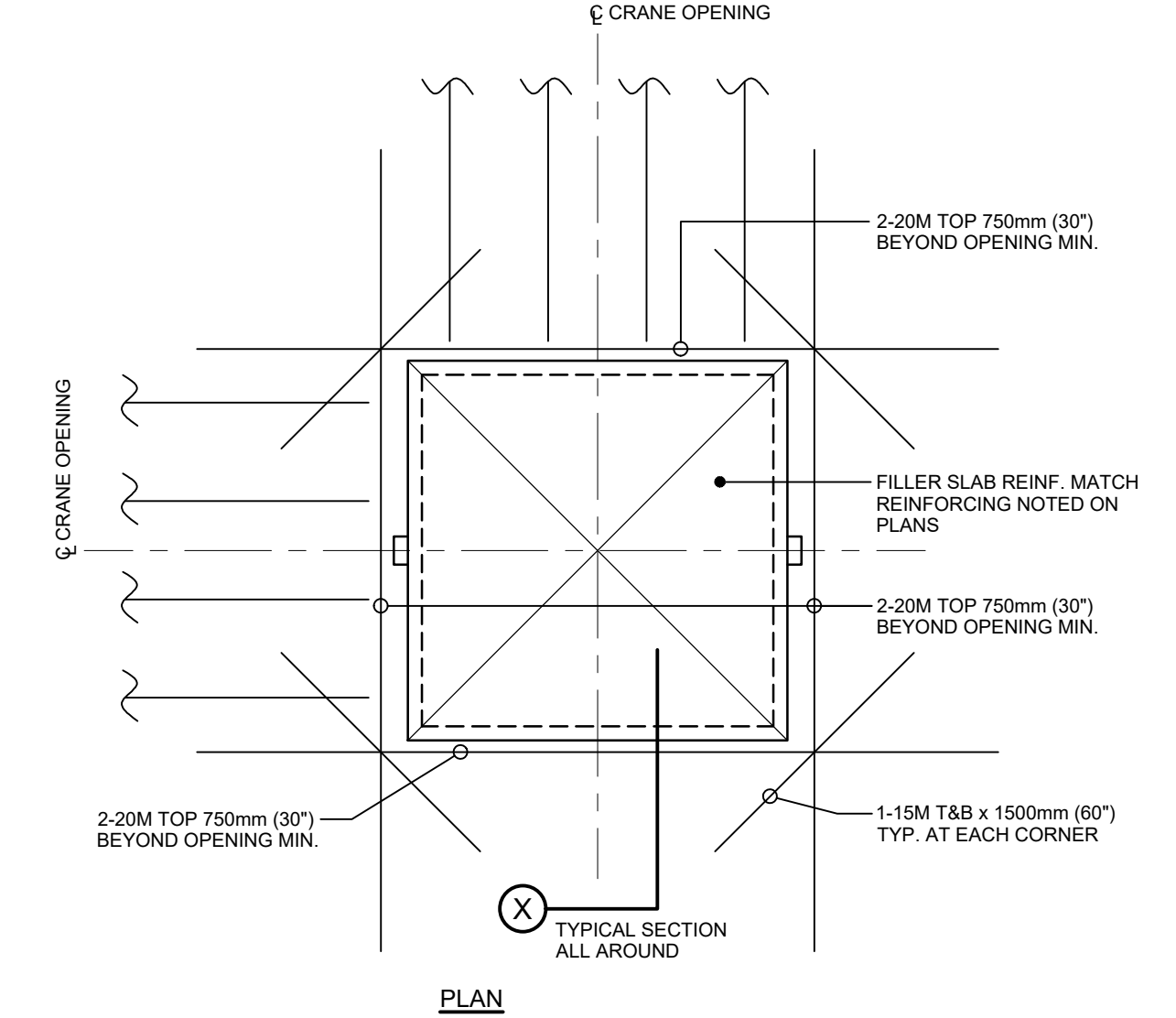
TYPICAL TRIMMING DETAIL OF CAST-IN-DUCTS IN SLAB U/N:



- TRIMMING NOTES:**
- SEE STRUCTURAL PLANS FOR APPROXIMATE SIZE AND LOCATION OF OPENINGS AND ARCH./MECH./ELECT. DRAWINGS FOR EXACT DIMENSIONS.
 - IF OPENINGS LARGER THAN 300mm (1'-0") WIDE ARE REQUIRED AND ARE NOT SPECIFICALLY NOTED ON THE DRAWINGS THE ENGINEER MUST BE INFORMED SO PROPER DETAILS CAN BE SUPPLIED.
 - UNLESS OTHERWISE NOTED OPENINGS SMALLER THAN 200x200mm (8"x8") DO NOT REQUIRE TRIMMER BARS.

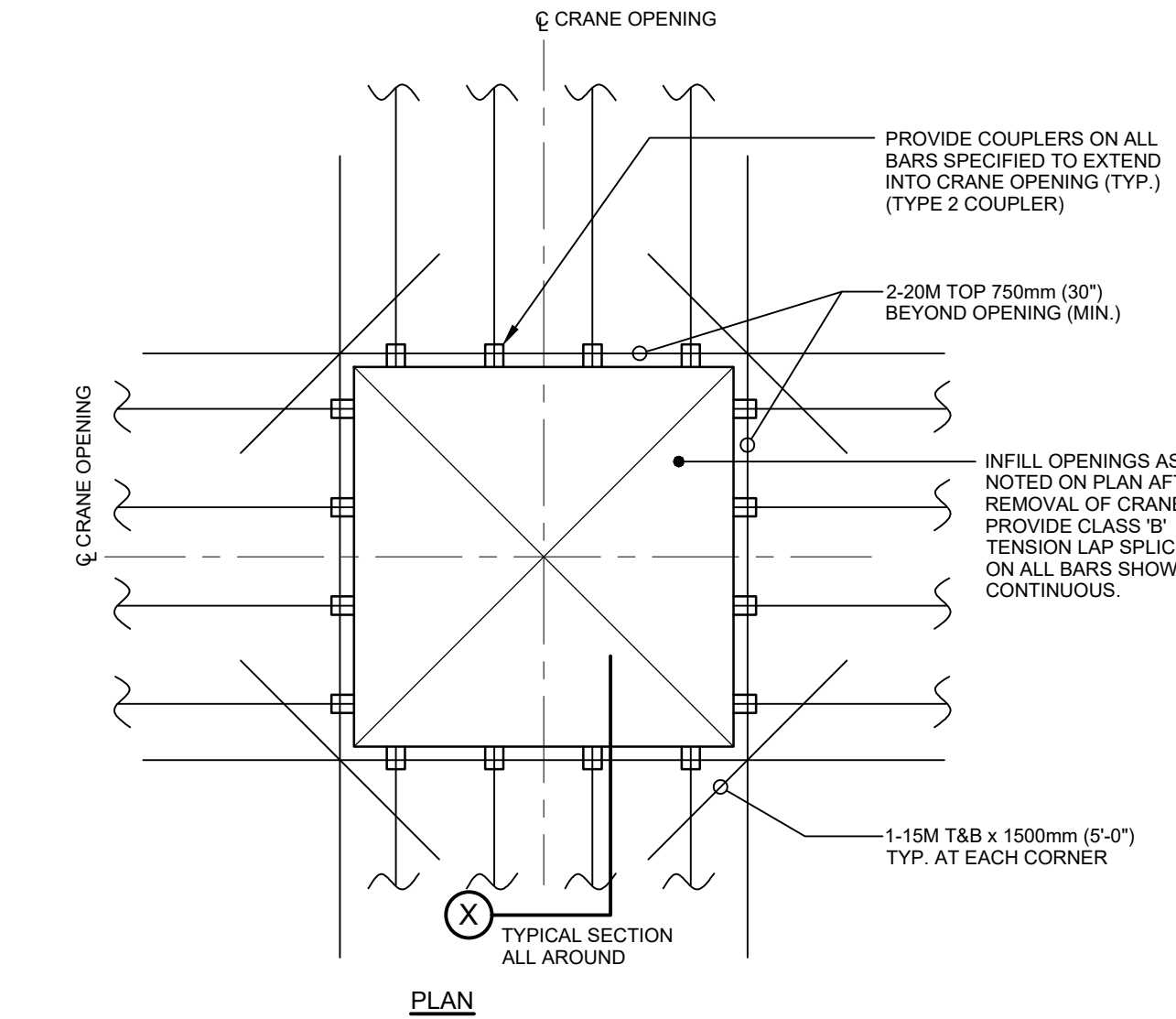
SLEEVES < 200mm(8") Ø

D03-25 TYPICAL CRANE OPENING (U/N)



- NOTES:**
- CUT BOTTOM REINFORCING STEEL RUNNING THROUGH CRANE OPENING.
 - PROVIDE ON EACH SIDE OF OPENING 1/2 OF AREA STEEL INTERRUPTED (CUT) BY THE CRANE OPENING 2-20M MIN. THESE BARS SHALL SPAN TO ADJACENT SUPPORTS.
-
- 10M @ 300(12") DOWELS
- 450(18")
- 50(2")
- ROUGHEN EDGE
- FILLER SLAB SAME THICKNESS AS FLOOR SLAB
- ADDITIONAL REINFORCING (SEE PLAN ABOVE)
- SECTION X**
- NOTE: LOCATION OF CRANE OPENING TO BE COORDINATED WITH STRUCTURAL CONSULTANT BEFORE PROCEEDING.

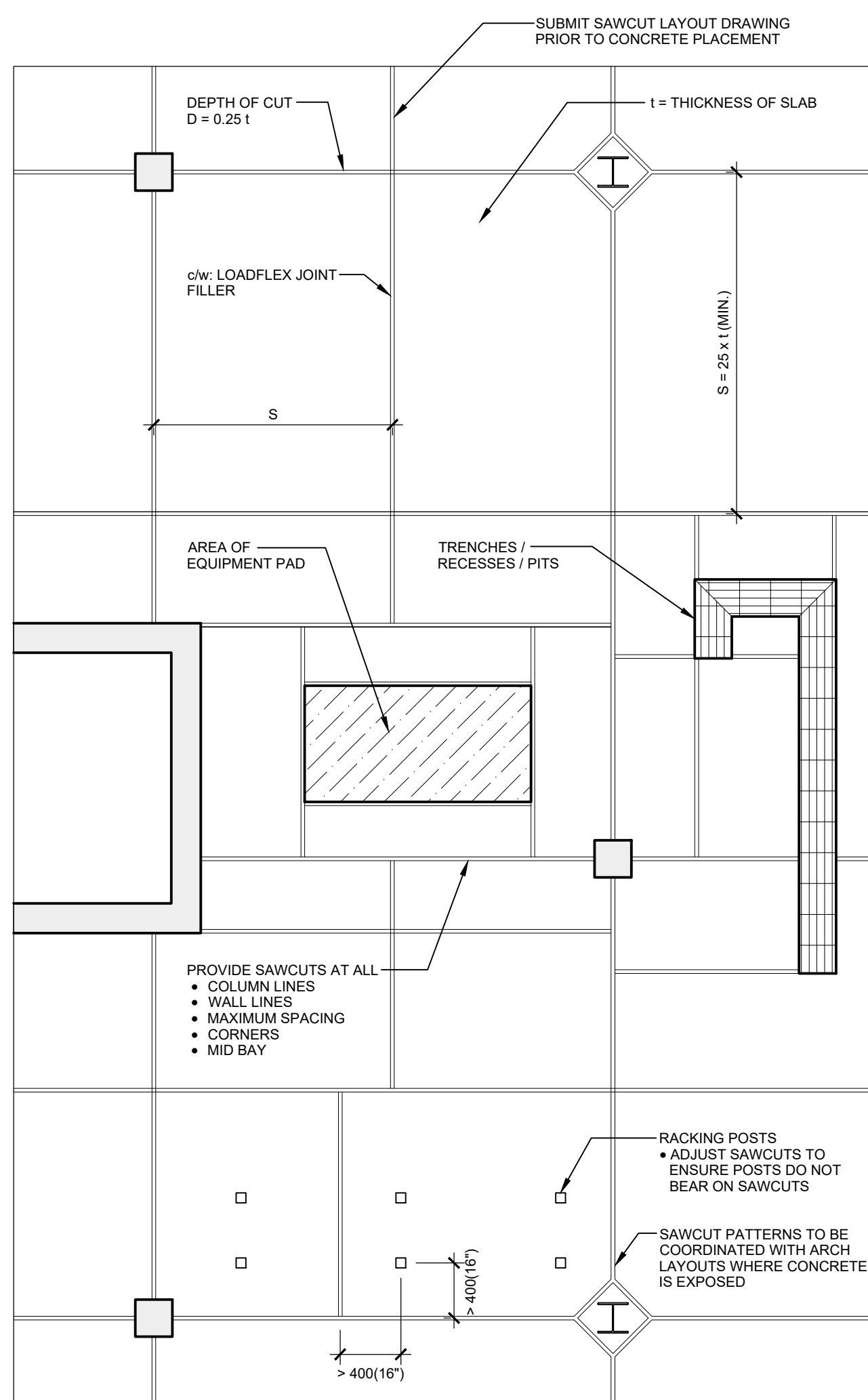
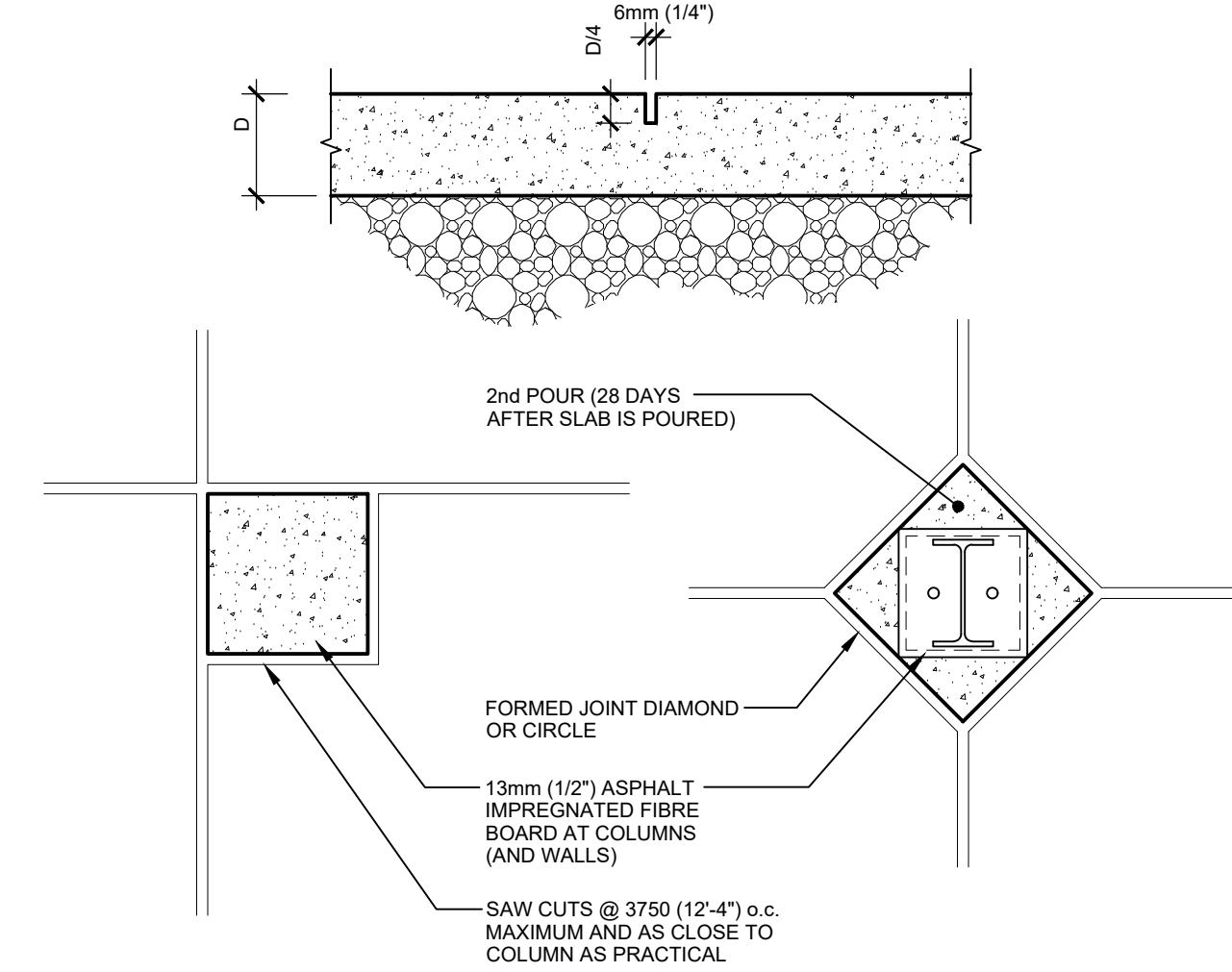
D03-25 TYPICAL CRANE OPENING (U/N)



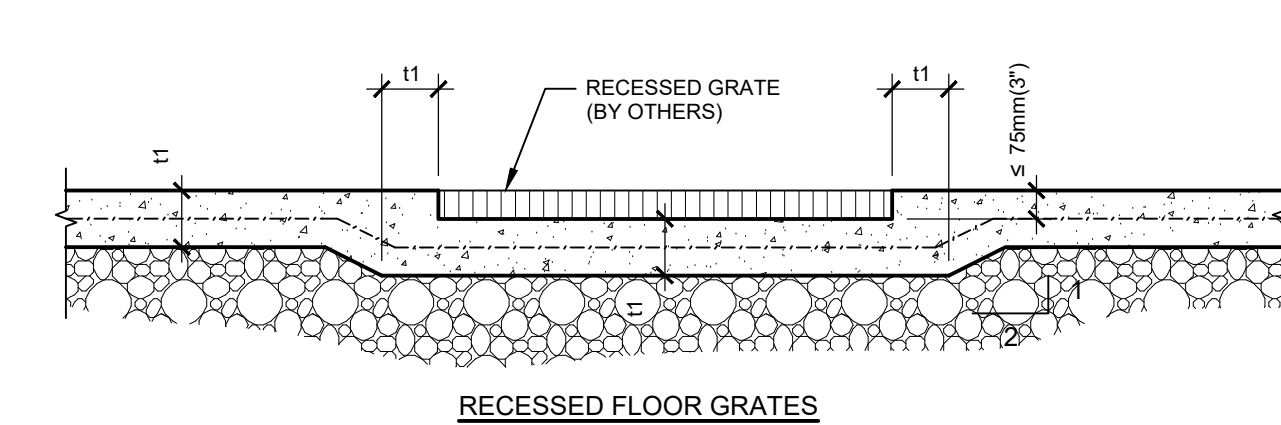
- NOTES:**
- CUT BOTTOM REINFORCING STEEL RUNNING THROUGH CRANE OPENING.
 - PROVIDE ON EACH SIDE OF OPENING 1/2 OF AREA STEEL INTERRUPTED (CUT) BY THE CRANE OPENING 2-20M MIN. THESE BARS SHALL SPAN TO ADJACENT SUPPORTS.
-
- PROVIDE COUPLERS ON ALL BARS SPECIFIED TO EXTEND INTO CRANE OPENING (TYP.)
- 50(2")
- ROUGHEN EDGE
- DRILL & EPOXY 10M @ 300(12") (x 400 LG.) (200mm (8") EMBEDMENT)
- INFL OPENINGS AS NOTED ON PLAN AFTER REMOVAL OF CRANE. PROVIDE CLASS 'B' TENSION LAP SPLICE ON ALL BARS SHOWN CONTINUOUS.
- ADDITIONAL REINFORCING (SEE PLAN ABOVE)
- SECTION X**
- NOTE: LOCATION OF CRANE OPENING TO BE CO-ORDINATED WITH STRUCTURAL CONSULTANT BEFORE PROCEEDING.

D03-26 SLAB ON GRADE CONTROL JOINTS AND SAWCUTS

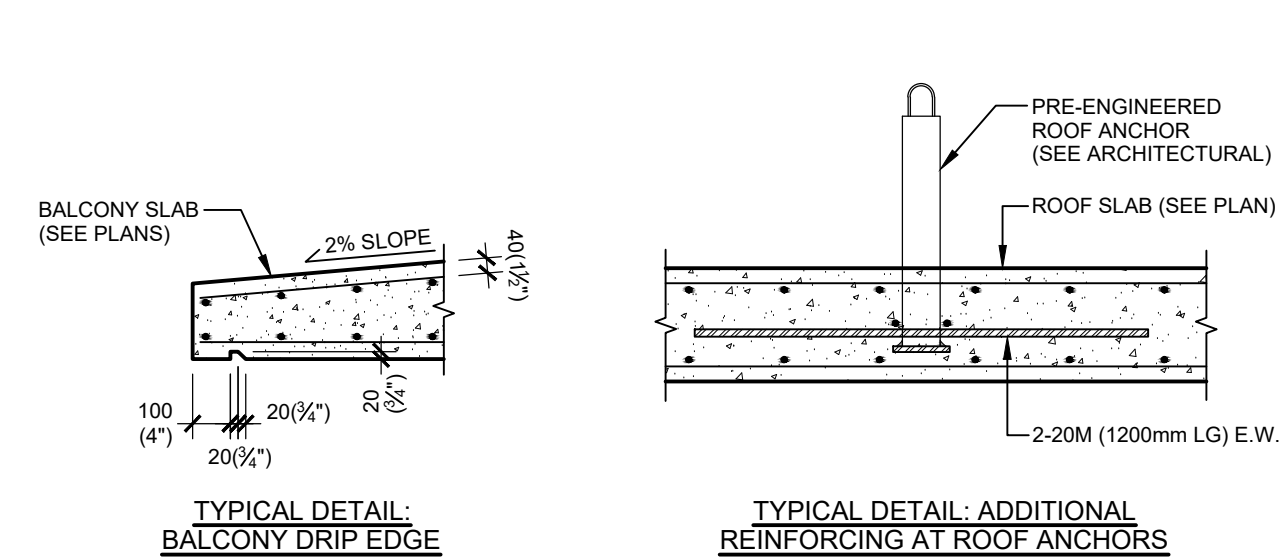
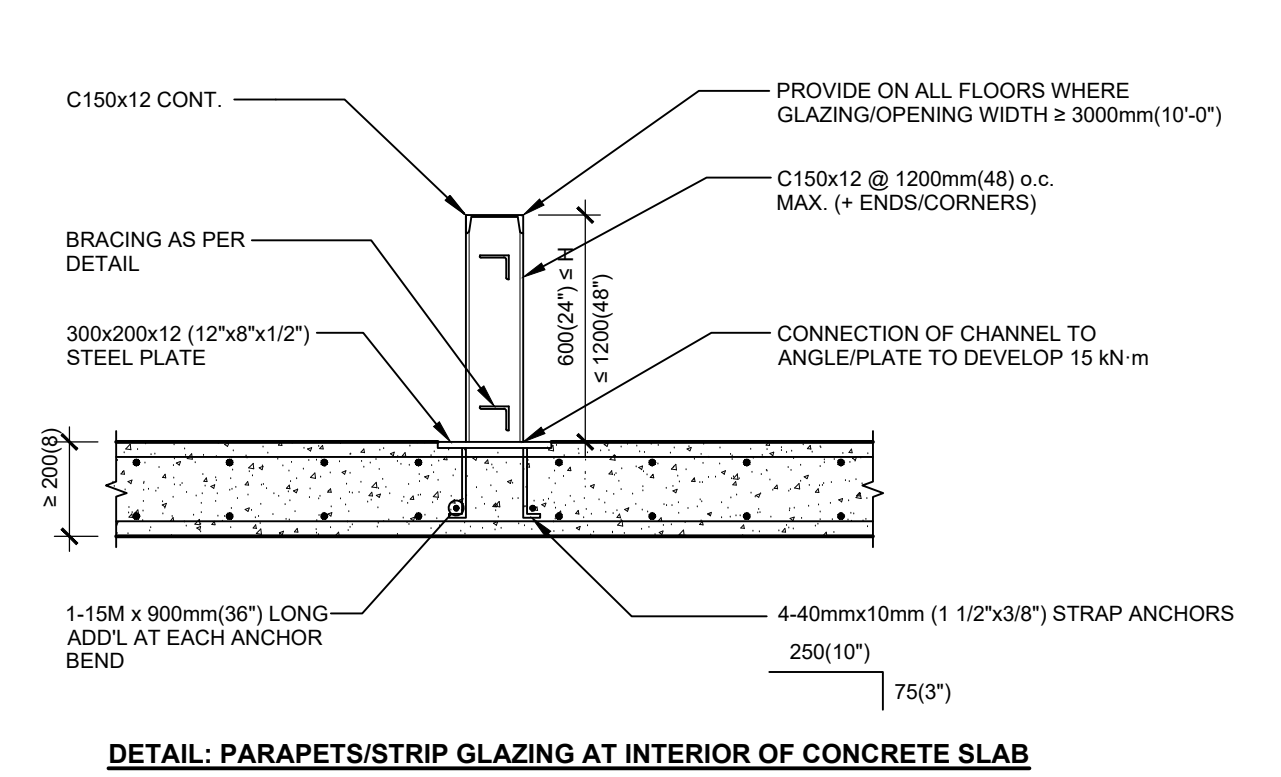
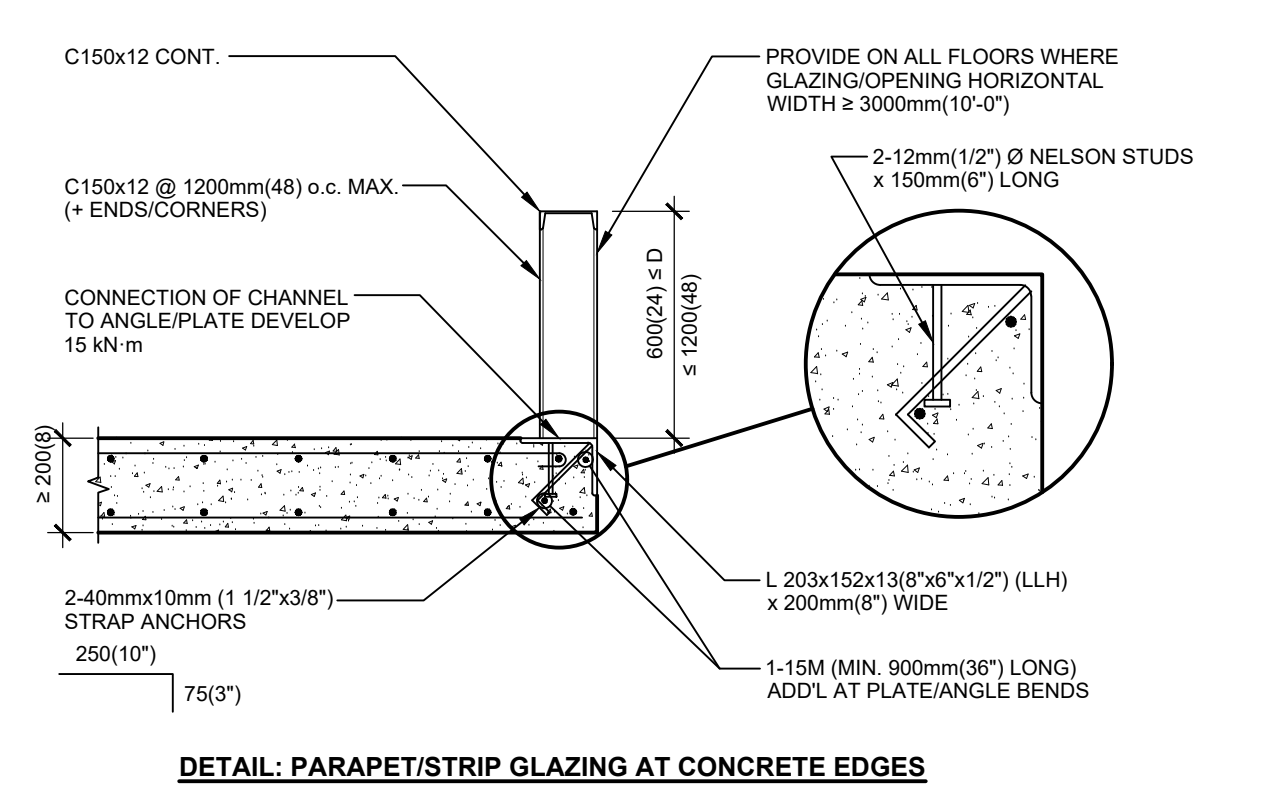
- SLAB ON GRADE TO BE PLACED ON COMPACTED GRANULAR MATERIAL IN STRICT ACCORDANCE WITH THE SOILS REPORT. COMPACTION TESTS ON FILL MATERIAL TO BE CARRIED OUT PRIOR TO SLAB ON GRADE PLACEMENT.
- PROVIDE APPROVED PRE-FORMED KEYED CONTROL JOINTS OR SAW CUTS (WITHIN 18 HOURS) AT MAXIMUM SPACING 3.75 m. CUT 1/3 DEPTH OF SLAB AND FILL WITH APPROVED MASTIC JOINT FILLER.
- BREAK BOND AT SURFACES OF CONTACT WITH OTHER CONCRETE (USE ASPHALT WATERPROOFING, HEAVY DUTY POLYETHYLENE OR SAND LAYER).
- PROVIDE 10mm ASPHALT IMPREGNATED FIBRE BOARD AND CAULKING AROUND ALL COLUMNS AND ALONG ALL WALLS.
- PROVIDE POLY FIBRE REINFORCING TYPICAL UNLESS OTHERWISE NOTED.
- PROVIDE CIRCULAR OR RECTANGULAR POCKETS AROUND COLUMNS. PLACE CONCRETE IN POCKET 4 WEEKS AFTER SLAB IS CONSTRUCTED.
- DO NOT PLACE SLAB ON GRADE IN ONE CONTINUOUS POUR IN LENGTHS EXCEEDING 30.0m IN EITHER DIRECTION.
- SUBMIT FOR REVIEW LAYOUT DRAWING WITH CONSTRUCTION JOINT LOCATIONS AND SAW CUT PATTERN.
- MAINTAIN MINIMUM SPECIFIED THICKNESS AT ALL DEPRESSIONS AND CHANGES IN ELEVATIONS.
- REFER TO ARCHITECTURAL DRAWINGS FOR EXTENT AND LOCATIONS OF ALL FINISHES AND DEPRESSIONS.



TYPICAL SAWCUT PATTERNS

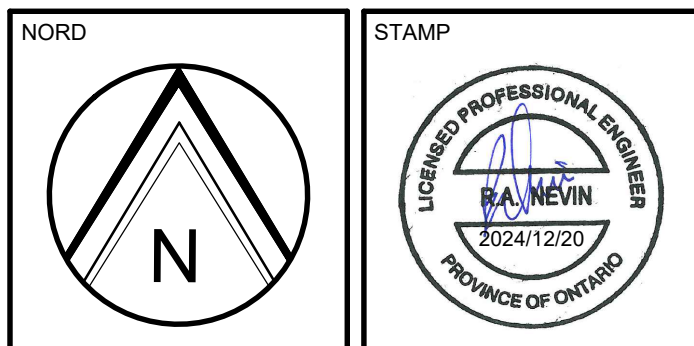


D03-27 SLAB EDGE DETAILS: PARAPETS / GLAZING



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1	DEC 20, 2024	ISSUED FOR PERMIT	AD
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PROJECT **Mercedes-Benz**
Star Motors of Ottawa
EXPANSION
400 West Hunt Club Rd,
Ottawa, Ontario

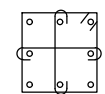
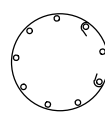
DRAWING
GENERAL NOTES AND
DETAILS

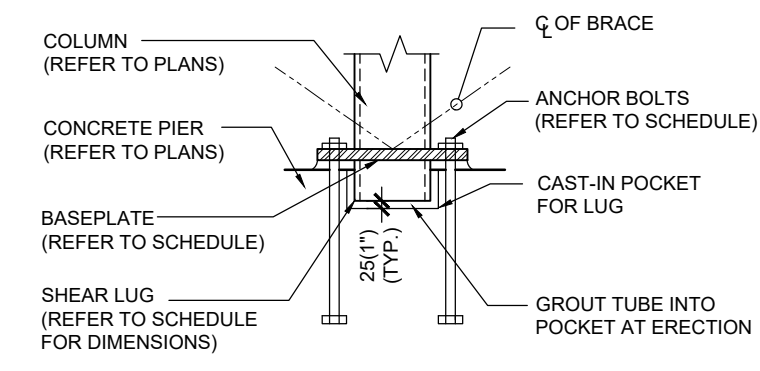
DRAWN:	A.D	DRAWING No.
DESIGNED:	R.N	
DATE:	DEC, 2024	
SCALE:	NTS	
PROJECT No:	23-0083	

S003

FOUNDATION WALL SCHEDULE				
MARK	DESCRIPTION	FLOOR	SIZE (W)	NOTES
FW1	TYPICAL EXTERIOR FOUNDATION WALL	FOOTING TO GROUND	300	10M @ 250 V.E.F. 10M @ 250 H.E.F. fc = 25 MPa, F-2
NOTES: 1. CONCRETE STRENGTHS: U/N: (MIN.) PARKING AREAS: 35 MPa, C-1 FROST WALLS (NO BASEMENT): 30 MPa, F-1 AREAWELLS: 35 MPa, C-1 RETAINING WALLS: 35 MPa, C-1 2. SEE SECTIONS / TYPICAL DETAILS FOR ADDITIONAL INFORMATION. 3. ALL WALLS TO BE CONTINUOUS IN VERTICAL / HORIZONTAL BARS BASEMENT WALLS: HORIZONTAL BARS: CLASS 'B' TENSION LAP (BOT. BARS) VERTICAL BARS: CLASS 'B' TENSION LAP (TOP BARS) AREAWELL WALLS: HORIZONTAL BARS: CLASS 'B' TENSION LAP (TOP BARS) VERTICAL BARS: CLASS 'B' TENSION LAP (TOP BARS) RETAINING WALLS: HORIZONTAL BARS: CLASS 'B' TENSION LAP (TOP BARS) VERTICAL BARS: V.I.F. (HIGH SIDE); CLASS 'B' TENSION LAP (TOP BARS) V.O.F. (LOW SIDE); CLASS 'B' TENSION LAP (BOT. BARS) OTHER WALLS (NOT SHEAR WALLS / BASEMENT / AREAWELL): HOR. / VERT. BARS: CLASS 'B' TENSION LAP (BOT. BARS) ALL WALLS: HOOK ALL VERTICALS 90° INTO TOP OF SLAB AT TERMINATION V.I.F.: BEND IN 24 BAR Ø MIN. 450mm V.O.F.: BEND IN 48 BAR Ø MIN. 700mm PROVIDE STANDARD 90° HOOKS TO HORIZONTALS AT ALL CORNERS / INTERSECTIONS 4. PROVIDE SHEAR KEY AT TOP / BOTTOM OF ALL LIFTS. 5. PROVIDE DOWELS TO MATCH VERTICALS IN ALL FOOTINGS. 6. LAYERING OF BARS: TYPICAL WALL AREAWELL WALL 7. REFER TO S300 DRAWINGS FOR SHEAR WALLS / CORE WALLS. SCHEDULE IS FOR WALLS THAT ARE NOT PART OF SFRS. 8. REFER TO ARCH. FOR STEPS IN FOUNDATION WALLS.				

FOOTING SCHEDULE		
MARK	SIZE (LxWxT)	NOTES
F1	1500x1500x300	5-15M B.E.W. $Q_{ult} \geq 100 \text{ kPa}$ $Q_{ult} \geq 150 \text{ kPa}$
F2	1700x1700x300	6-15M T&B E.W. $Q_{ult} \geq 100 \text{ kPa}$ $Q_{ult} \geq 150 \text{ kPa}$
F3	600x300 DP	TYPICAL STRIP FOOTING 3-15M CONT. $Q_{ult} \geq 100 \text{ kPa}$ $Q_{ult} \geq 150 \text{ kPa}$
NOTES: 1. ALL FOOTINGS TO BEAR ON SUITABLE BEARING STRATA AS APPROVED BY GEOTECHNICAL ENGINEER/IN ACCORDANCE WITH GEOTECHNICAL REPORT WITH MINIMUM BEARING PRESSURES NOTED IN TABLE. 2. PROVIDE MINIMUM 1500(5'-0") FROST COVER TO ALL FOOTINGS EXPOSED TO EXTERIOR CONDITIONS U/N ON DRAWINGS/GEOTECHNICAL REPORT. 3. CONCRETE STRENGTH: fc = MPa(psi) U/N 4. TOPS OF INTERIOR FOOTINGS/WALL/PIERS TO BE A MINIMUM OF 300(12") BELOW THE TOP OF THE SLAB ON GRADE. STEP DOWN INTERIOR FOOTINGS TO EXTERIOR FOOTINGS AS REQUIRED, FINAL BEARING ELEVATIONS TO BE BASED ON GEOTECHNICAL REPORT DATA U/N. 5. FOOTING AND BOTTOM OF WALL ELEVATIONS TO BE ESTABLISHED FROM PLANS AND GEOTECHNICAL REPORT. WALLS/COLUMNS ARE TO BE TERMINATED SUCH THAT THEY ARE FOUNDED ON SUITABLE BEARING STRATA (WITH APPROPRIATE FROST COVER) APPROVED BY GEOTECHNICAL ENGINEER ON SITE. REFER ALSO TO GEOTECHNICAL REPORT. 6. FOOTINGS ARE TO BE LOWERED AS REQUIRED IN THE AREAS OF PITS/SHAFTS AT FOUNDATION LEVEL SUCH THAT THE U/S OF THE PIT/SHAFT IS AT THE TOP OF THE FOOTING. CONTRACTOR IS RESPONSIBLE FOR COORDINATION OF ELEVATIONS/STEPS IN FOOTINGS. CONTRACTOR IS REQUIRED TO PREPARE FOOTING ELEVATION DRAWINGS PRIOR TO EXCAVATION.		

PIER SCHEDULE		
MARK	SIZE	REINFORCING
P1	450x450	8 - 20M VERT. + DOWELS 3 - 10M TIES @ 300 o.c. 
P2	500 Ø	CANOPY 8 - 20M VERT. FULL HEIGHT 1 - 10M TIES @ 300 
NOTES: 1. TOPS OF PIERS TO BE -300mm (-12") BELOW TOP OF SLAB ON GRADE (U.N.O.). 2. TOPS OF EXTERIOR PIERS TO BE AT +/- 150mm ABOVE FINISHED GRADE (REFER TO ARCH.) 3. PIERS DIMENSIONS ARE TO BE CENTRED ON SUPPORTED COLUMNS (U.N.O.). INCREASE CONCRETE SIZE TO SUIT FOUNDATION WALL OFFSETS. 4. VERTICAL BARS IN PIERS MAY BE LAPPED WITH COMPRESSION LAPS WHERE NO BRACE/MOMENT FRAMES ARE PRESENT. WHERE BRACE/MOMENT FRAMES ARE PRESENT VERTICAL BARS ARE TO BE EXTEND TO FULL HEIGHT ABOVE FOOTING TO TOP OF PIERS (NO LAPS ARE PERMITTED UNLESS APPROVED BY ENGINEER IN WRITING). CLASS 'B' TENSION LAPS (MIN. 1.5d) MAY BE USED WHERE HEIGHT OF PIER EXCEEDS 2400 (8'-0"). 5. CONCRETE STRENGTH: fc = 25 MPa EXTERIOR OR EXTERIOR WALL: CLASS F-2 INTERIOR: CLASS N 6. PROVIDE ADDITIONAL GROUP OF TIES AT TOP 150mm(6") SPACING		

BASEPLATE SCHEDULE: SINGLE STOREY BUILDINGS														
MARK	SIZE (LxWxT)	NOTES												
Bx1	300x300x20	TYPICAL COLUMN 4 - 16 Ø ANCHOR BOLTS 												
Bx2	400x400x20	BRACE FRAMES 4 - 25 Ø SEISMIC HEADED ANCHORS SHEAR LUG 50mm(h) x 12.7mm(t) x 400(g) 												
Bx3	400 Ø x 20mm THICK	4 - 16 Ø A307 ANCHOR BOLTS 												
NOTES: 1. LENGTH OF ANCHORS IS EMBEDMENT LENGTH. FABRICATOR TO PROVIDE ADDITIONAL LENGTH AS REQUIRED FOR THREADS/TOLERANCES, ETC. 2. ALL ANCHORS TO BE CAST-IN (CONCRETE) OR GROUTED INTO PLACE (MASONRY). 3. PROVIDE MIN. 25(1") THICK GROUT BED BELOW BASE PLATE U/N. 4. SEISMIC SHEAR LUG DETAIL: (REFER TO SCHEDULE FOR LOCATIONS)  5. SEISMIC HEADED ANCHORS: FOLLOWING OUTLINES MINIMUM WASHER PLATE (c/w: NUT ABOVE/BELOW PLATE-TACK WELD NUT TO PLATE) SIZES FOR BOLT ENDS: <table><tr><td>16mmØ: 52x52x16mm</td><td>(5/8"Ø: 2"x2"x5/8")</td></tr><tr><td>19mmØ: 63x63x16mm</td><td>(3/4"Ø: 2 1/2"x2 1/2"x5/8")</td></tr><tr><td>25mmØ: 76x76x20mm</td><td>(1"Ø: 3"x3"x3/4")</td></tr><tr><td>28mmØ: 82x82x20mm</td><td>(1 1/8"Ø: 3 1/4"x3 1/4"x3/4")</td></tr><tr><td>32mmØ: 89x89x20mm</td><td>(1 1/4"Ø: 3 1/2"x3 1/2"x3/4")</td></tr><tr><td>38mmØ: 102x102x20mm</td><td>(1 1/2"Ø: 4"x4"x3/4")</td></tr></table> 6. ANCHOR BOLT EMBEDMENT LENGTHS HAVE BEEN DEVELOPED IN ACCORDANCE WITH CAN/CSA A23.3-04 CLAUSES 7.1.4, ANNEX D, 12.2, AND 21.2.7. DEPTHS ARE BASED ON MINIMUM EMBEDMENT AND THE DEVELOPMENT OF THE PIER REINFORCING STEEL IN TENSION ABOVE THE CONE OF FAILURE CREATED BY THE BOLT HEAD.			16mmØ: 52x52x16mm	(5/8"Ø: 2"x2"x5/8")	19mmØ: 63x63x16mm	(3/4"Ø: 2 1/2"x2 1/2"x5/8")	25mmØ: 76x76x20mm	(1"Ø: 3"x3"x3/4")	28mmØ: 82x82x20mm	(1 1/8"Ø: 3 1/4"x3 1/4"x3/4")	32mmØ: 89x89x20mm	(1 1/4"Ø: 3 1/2"x3 1/2"x3/4")	38mmØ: 102x102x20mm	(1 1/2"Ø: 4"x4"x3/4")
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38mmØ: 102x102x20mm	(1 1/2"Ø: 4"x4"x3/4")													

STEEL COLUMN SCHEDULE		
MARK	SIZE	NOTES
C1	HSS 152 x 152 x 6.4	TYPICAL INTERIOR COLUMN CLASS 'C' A500
NOTES: 1. REFER TO PLANS FOR ELEVATIONS AND ORIENTATIONS. 2. ALL HSS COLUMNS TO BE CLASS 'C' A500. 3. CONTRACTOR TO COORDINATE LENGTHS OF COLUMNS BEARING AT PIERS AND INTERIOR FOOTINGS.		

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REQUIRED SUBMITTALS

THE FOLLOWING ITEMS SHALL BE SUBMITTED TO THE ENGINEER FOR REVIEW PRIOR TO FABRICATION.

ITEM	REQ'D SUBMITTAL	ENGINEER'S STAMP REQ'D	NOTES
REBAR SHOP DRAWINGS	YES	NO	
CONCRETE MIX DESIGNS	YES	NO	
MASONRY GROUT MIX DESIGN	NO	NO	
BLOCK MILL REPORT	NO	NO	
STRUCTURAL STEEL SHOP DRAWINGS	YES	YES	FOR CONNECTIONS / OWSJ ONLY
I-SPAN JOIST SHOP DRAWINGS	NO	YES	
ENGINEERED LUMBER / WOOD TRUSSES	NO	YES	
MISCELLANEOUS STEEL SHOP DRAWINGS	YES	YES	STAMP FOR STAIRS, LADDERS AND GUARDS
STEEL DECK SHOP DRAWINGS	YES	YES	
FALL ARREST ANCHORS	NO	YES	
SEISMIC RESTRAINT OF NON-STRUCTURAL ITEMS	YES	YES	
STEEL STUDS	YES	YES	
PRECAST CONCRETE	NO	YES	

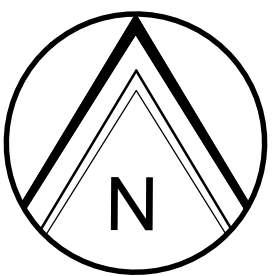
TESTING / PERIODIC REVIEW / INSPECTION

THE FOLLOWING ITEMS REQUIRE TESTING OR INSPECTION BY A CERTIFIED INDEPENDENT TESTING OR INSPECTION AGENCY UNLESS NOTED OTHERWISE. THE AGENCY SHALL SEND COPIES OF ALL STRUCTURAL TESTING AND INSPECTION REPORTS TO THE ENGINEER FOR REVIEW.

ITEM	REQ'D	COMMENTS
SOIL BEARING CAPACITY	YES	BY SOILS ENGINEER
REINFORCING STEEL PLACEMENT	YES	INSPECT FINAL PLACEMENT
CONCRETE COMPRESSIVE TESTS	YES	MIN. 2 SETS PER 100 CUBIC METRES
CONCRETE SLUMP	YES	
STRUCTURAL STEEL BOLTING	YES	INSPECT ALL FIELD WELDS
GENERAL STEEL REVIEW	NO	
STRUCTURAL STEEL WELDING	YES	WELDING INSPECTOR TO REVIEW ALL FIELD WELDS
MORTAR CUBES	YES	

GENERAL CONTRACTOR TO NOTIFY EOR 48 HRS PRIOR TO ANY REQUIRED REVIEW.

1	DEC 20, 2024	ISSUED FOR PERMIT	AD
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STAMP

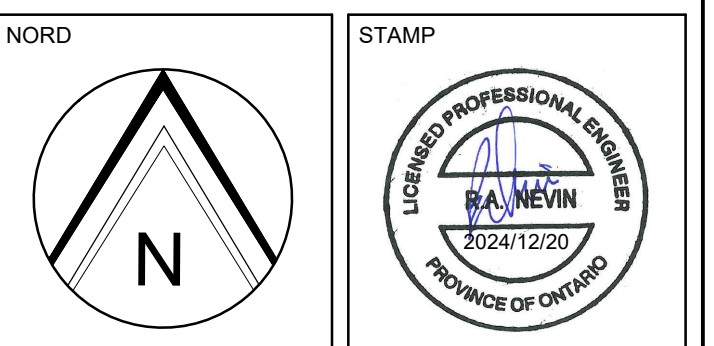
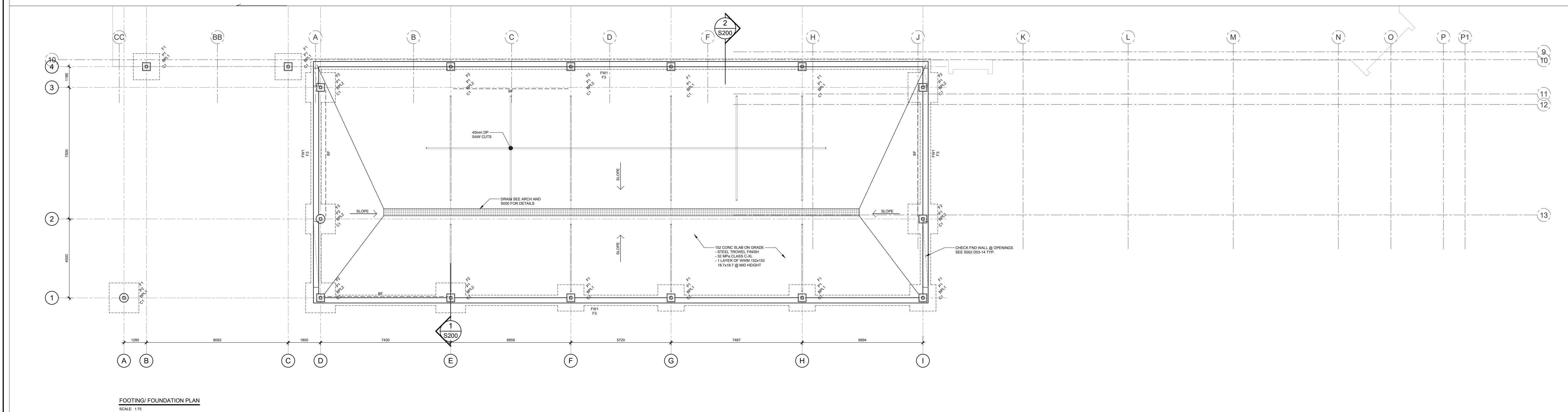
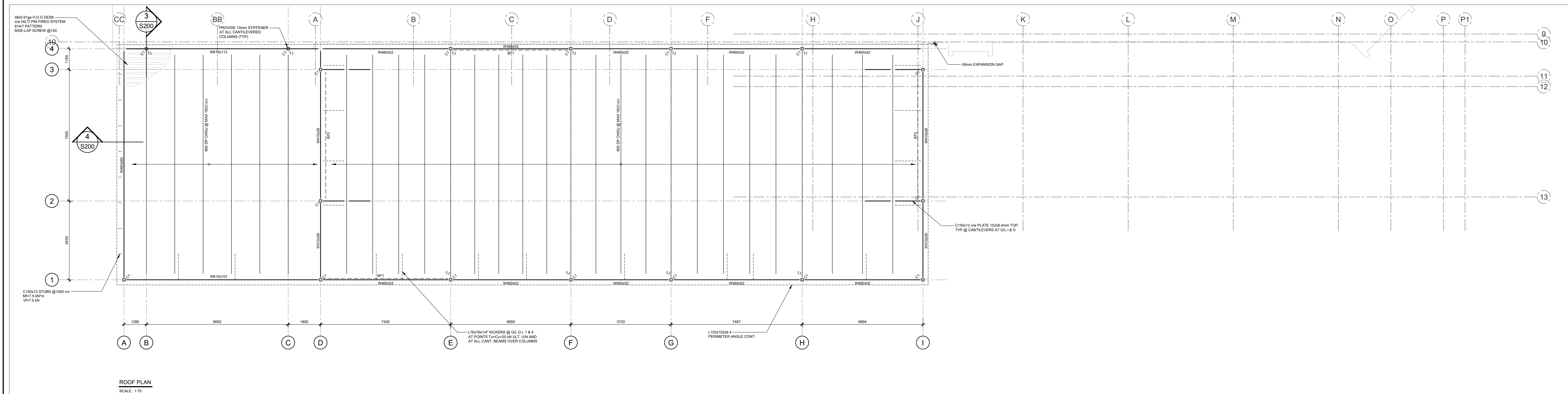


PROJECT **Mercedes-Benz
Star Motors of Ottawa
EXPANSION**
400 West Hunt Club Rd,
Ottawa, Ontario

DRAWING
SCHEDULES

DRAWN: A.D	DRAWING No.
DESIGNED: R.N	S004
DATE: DEC, 2024	
SCALE: NTS	
PROJECT No: 23-0083	

PROJECT Star Motors of Ottawa EXPANSION 400 West Hunt Club Rd, Ottawa, Ontario			
DRAWING PLAN VIEW			
DRAWN:	A.D	DRAWING No.	S100
DESIGNED:	R.N	S100	
DATE:	DEC. 2024		
SCALE:	NTS		
PROJECT No:	23-0083		



PROJECT **Mercedes-Benz**
Star Motors of Ottawa
EXPANSION

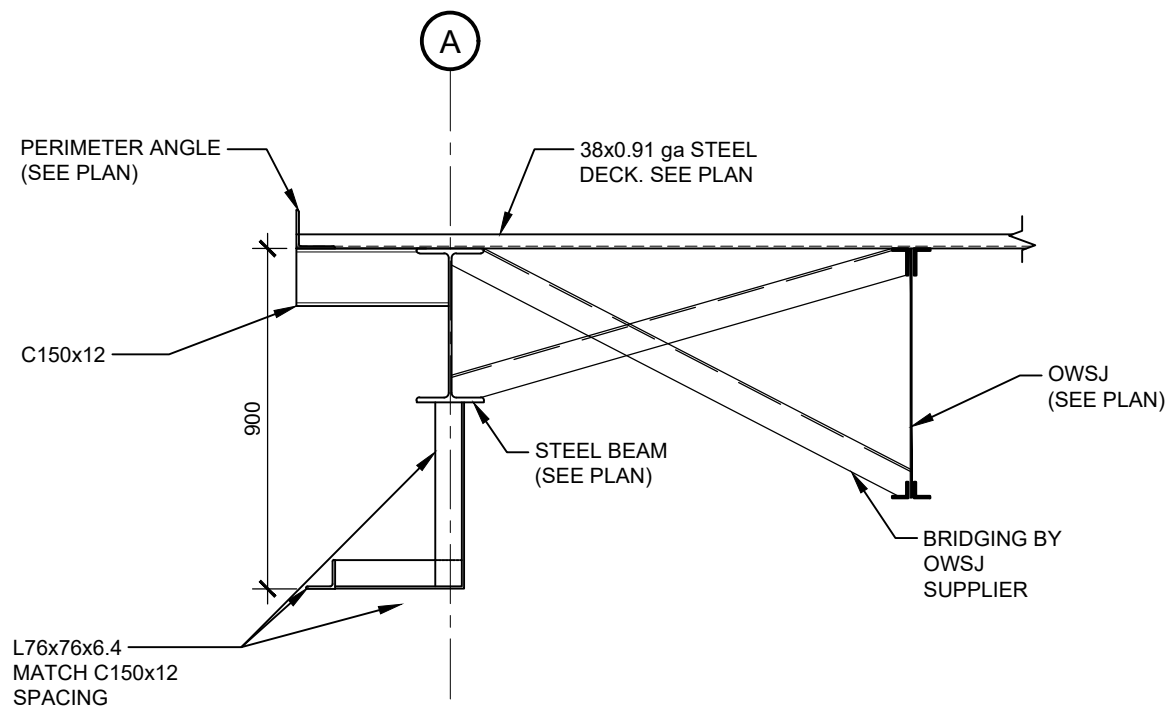
400 West Hunt Club Rd.,
Ottawa, Ontario

DRAWING

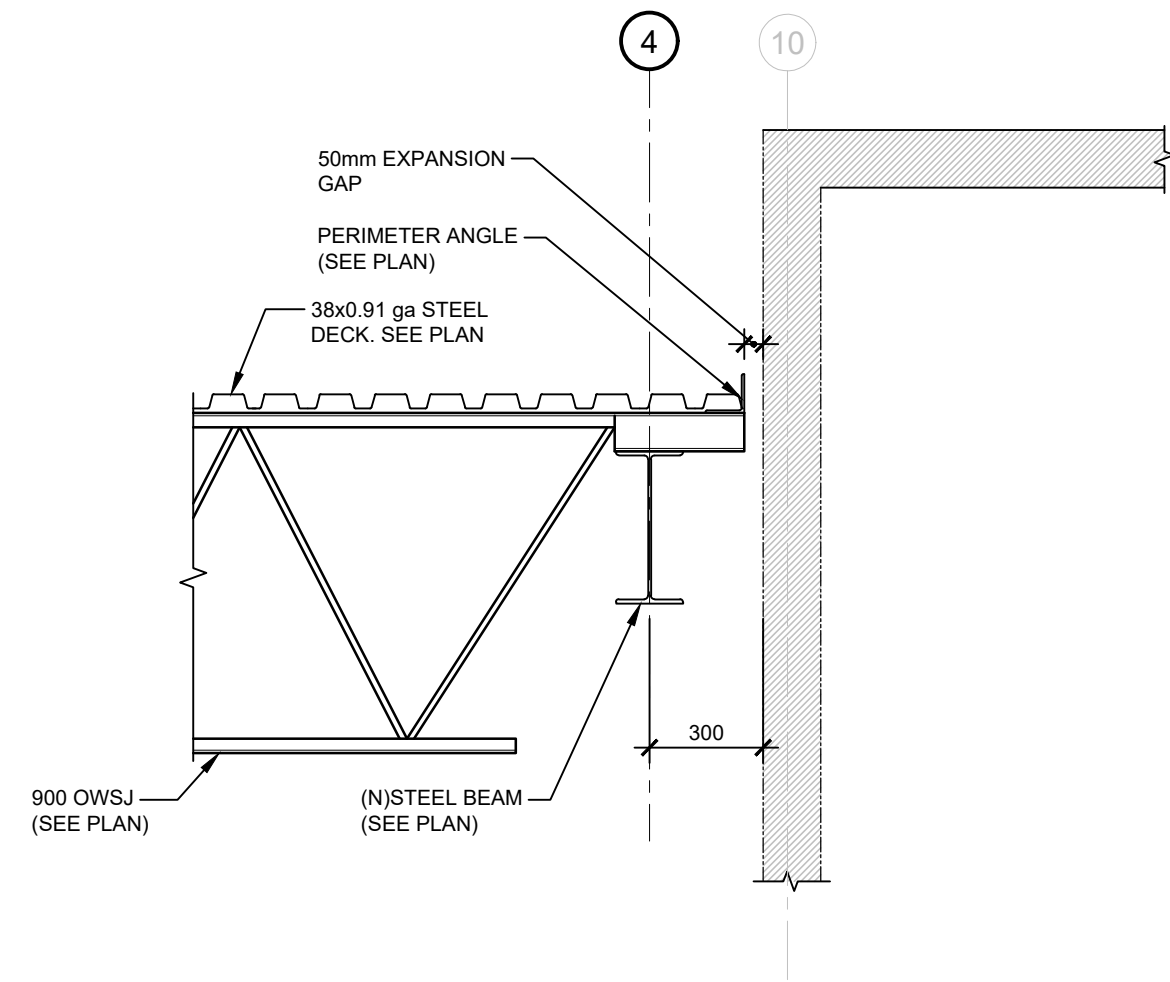
PLAN VIEW

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DESIGNED:	R.N	
DATE:	DEC. 2024	
SCALE:	NTS	
PROJECT No:	23-0083	

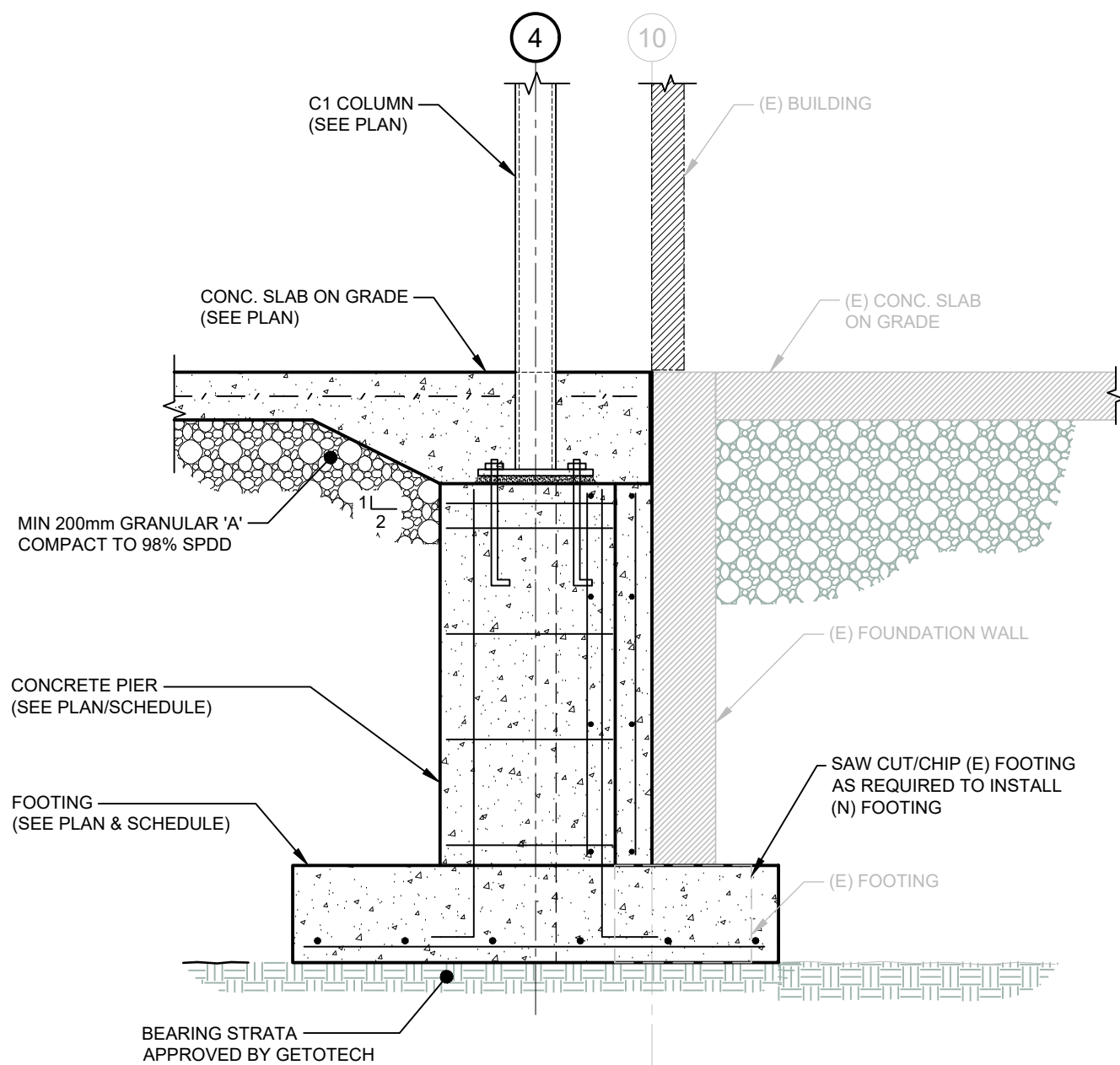
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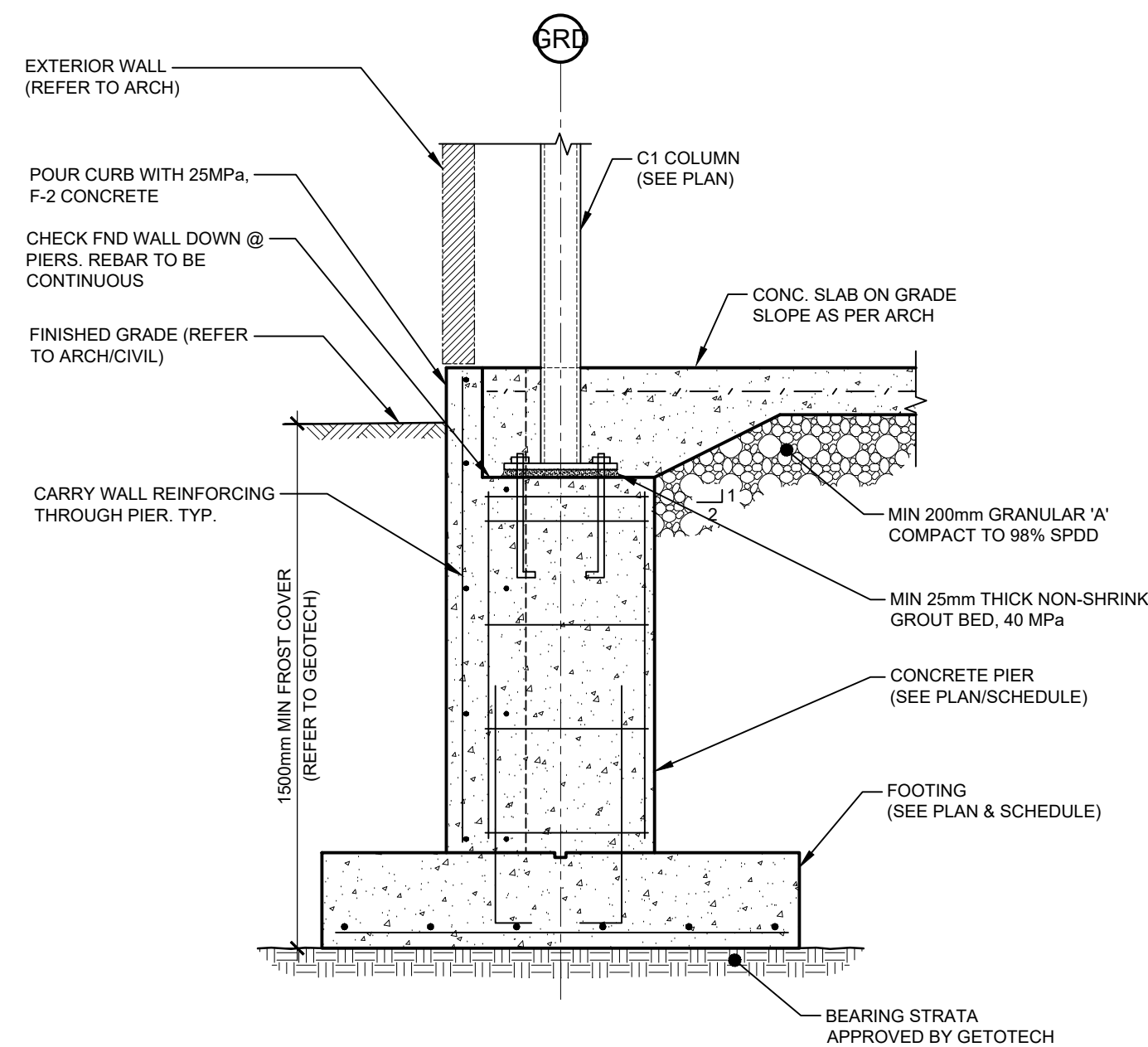
4 SECTION: TYPICAL ROOF JOIST AT EXISTING (JOIST PARRALLEL)
S200 SCALE 1:20



3 SECTION: TYPICAL ROOF JOIST AT EXISTING (JOIST PERPENDICULAR)
S200 SCALE 1:20

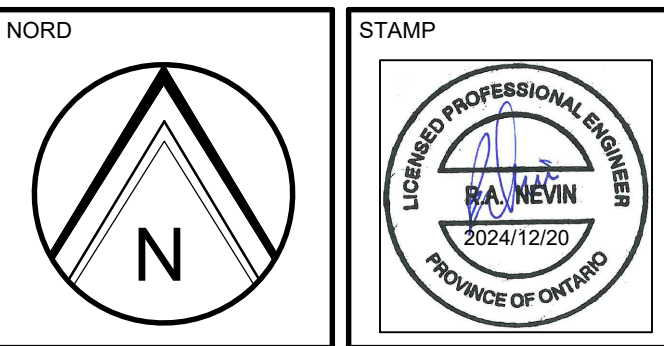


2 SECTION: PIER AT EXISTING FOUNDATION
S200 SCALE 1:20



1 SECTION: TYPICAL PIER AT FOUNDATION WALL
S200 SCALE 1:20

No.	DATE	ISSUED FOR PERMIT	AD
1	DEC 20, 2024	ISSUED FOR PERMIT	AD

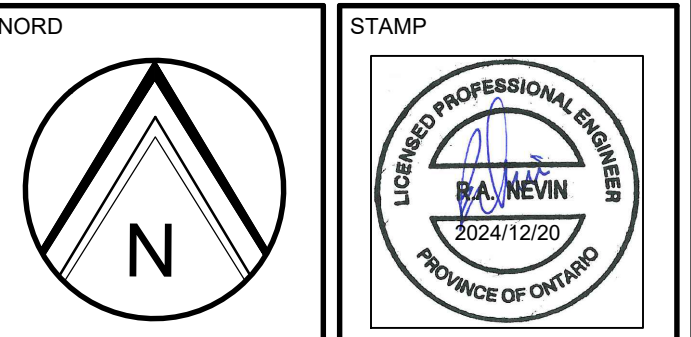
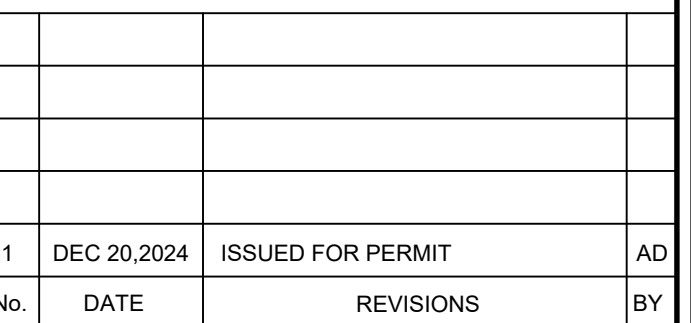
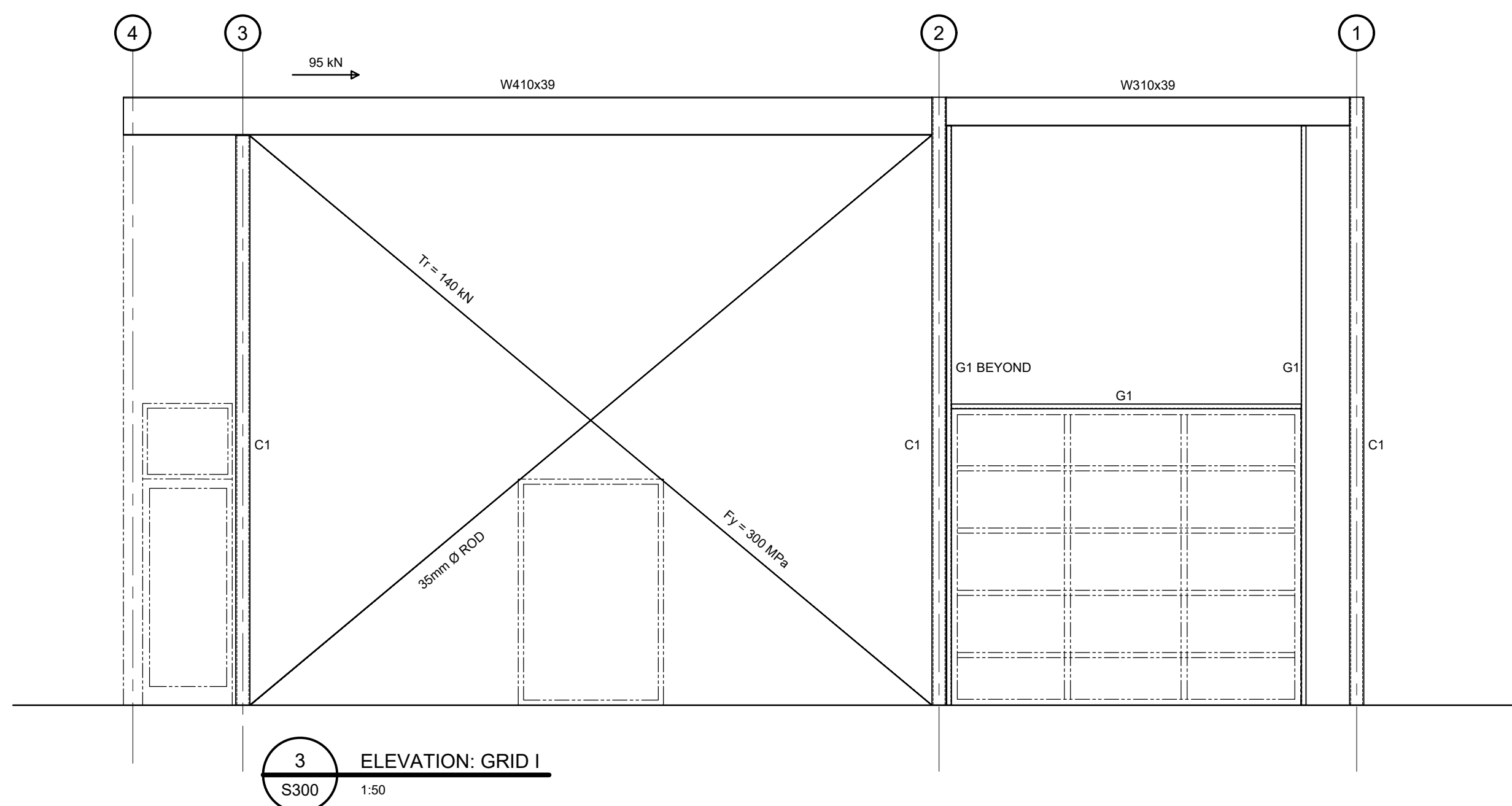
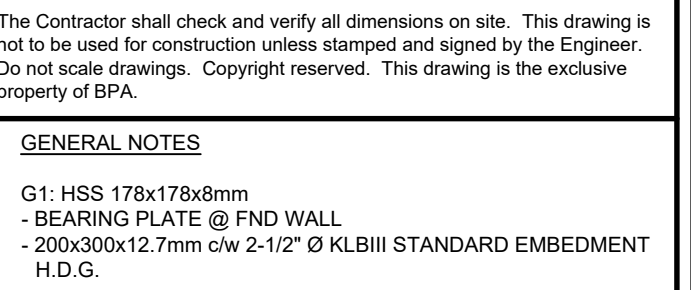


PROJECT
**Mercedes-Benz
Star Motors of Ottawa
EXPANSION**
400 West Hunt Club Rd,
Ottawa, Ontario

DRAWING
SECTIONS

DRAWN:	A.D	DRAWING No.
DESIGNED:	R.N	
DATE:	DEC. 2024	
SCALE:	NTS	
PROJECT No:	23-0083	

S200



PROJECT **Mercedes-Benz
Star Motors of Ottawa
EXPANSION**

400 West Hunt Club Rd,
Ottawa, Ontario

DRAWING

BRACE FRAMES

DRAWN:	A.D	DRAWING No. S300
DESIGNED:	R.N	
DATE:	DEC. 2024	
SCALE:	NTS	
PROJECT No:	23-0083	